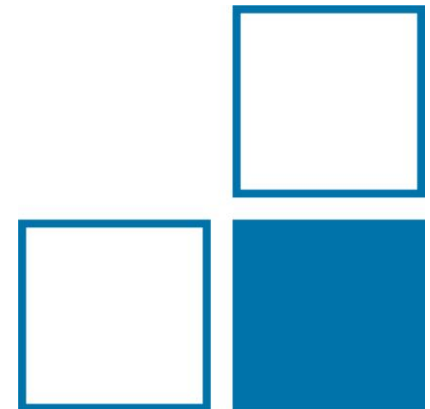


Unsicherheitsquantifizierung von CFD Simulationen

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On-site calibration of flow meters in district heating systems

Partners:

OPTOLUTION
messtechnische lösungen

ILA Intelligent Laser
Applications GmbH

VATTENFALL

Technische
Universität
Berlin

PTB

EnEff:Wärme
Forschung für
energieeffiziente Wärme- und Kältenetze

Gefördert durch:

 Bundesministerium
für Wirtschaft
und Energie

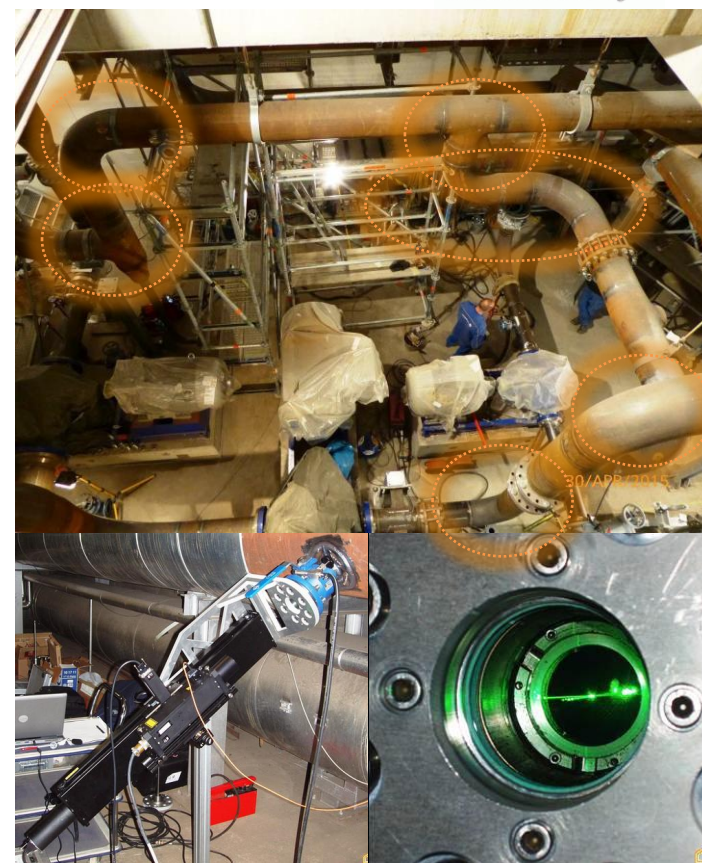
aufgrund eines Beschlusses
des Deutschen Bundestages

Goal:

on-site calibration of installed flow meters in the Berliner district heating system

Challenge:

- Measurement of one path with Laser-Doppler-velocimetry
- limited access to measurement positions
- huge diameters (> 400 mm), high temperatures (>80°C), high Volume Flow
- Combinations of elbows and T-Junctions disturb flow profiles in front of the flow meter

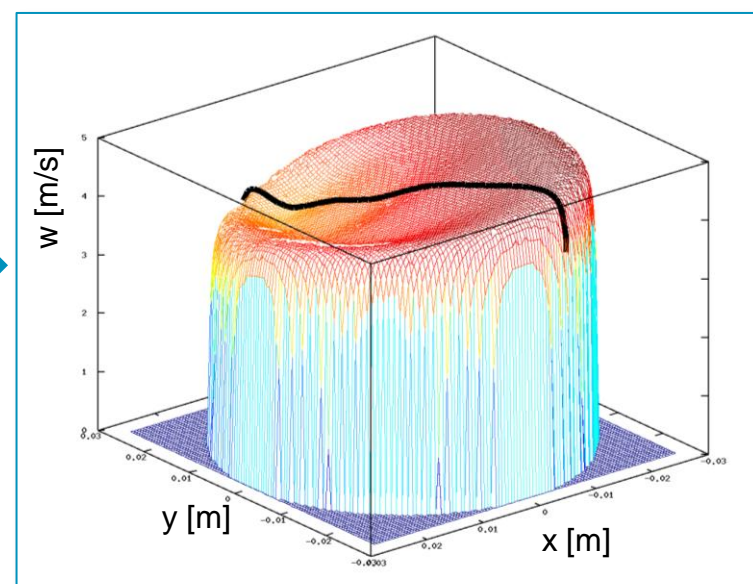
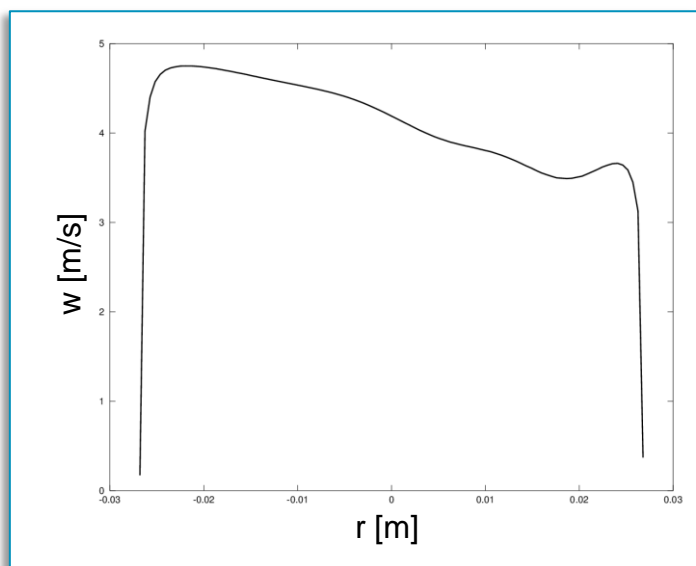


→ **non symmetric Profiles**

→ **huge error in integration of only one path**

Idea:

- Measurement of one path with Laser-Doppler-Velocimetry
- CFD-Simulation of flow downstream a disturbing geometry
- Reconstruction of the flow profile on the measurement cross section



volume flow Q



uncertainty?

Sensitivity of a double elbow out-of-plane

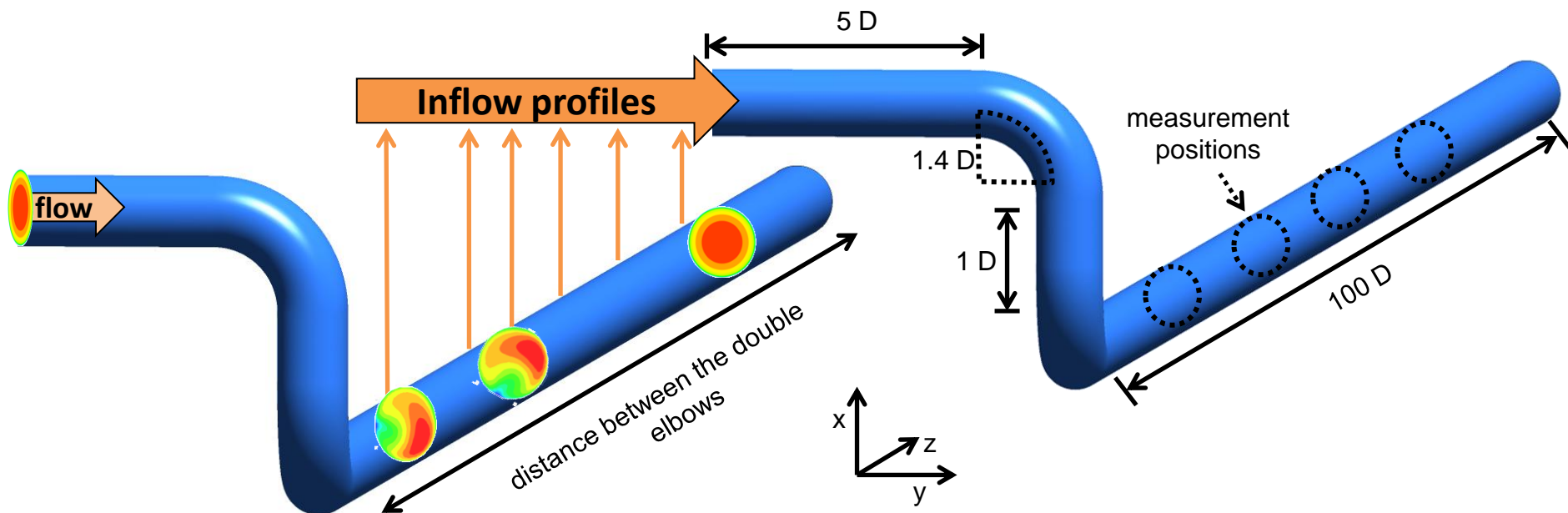
- Double elbow with ideal inlet profile
- Two Double elbows out-of-plane in a row:
 - Double elbows creating swirl with **same** direction
 - Double elbows creating swirl with **opposite** directions

Numerical set up:

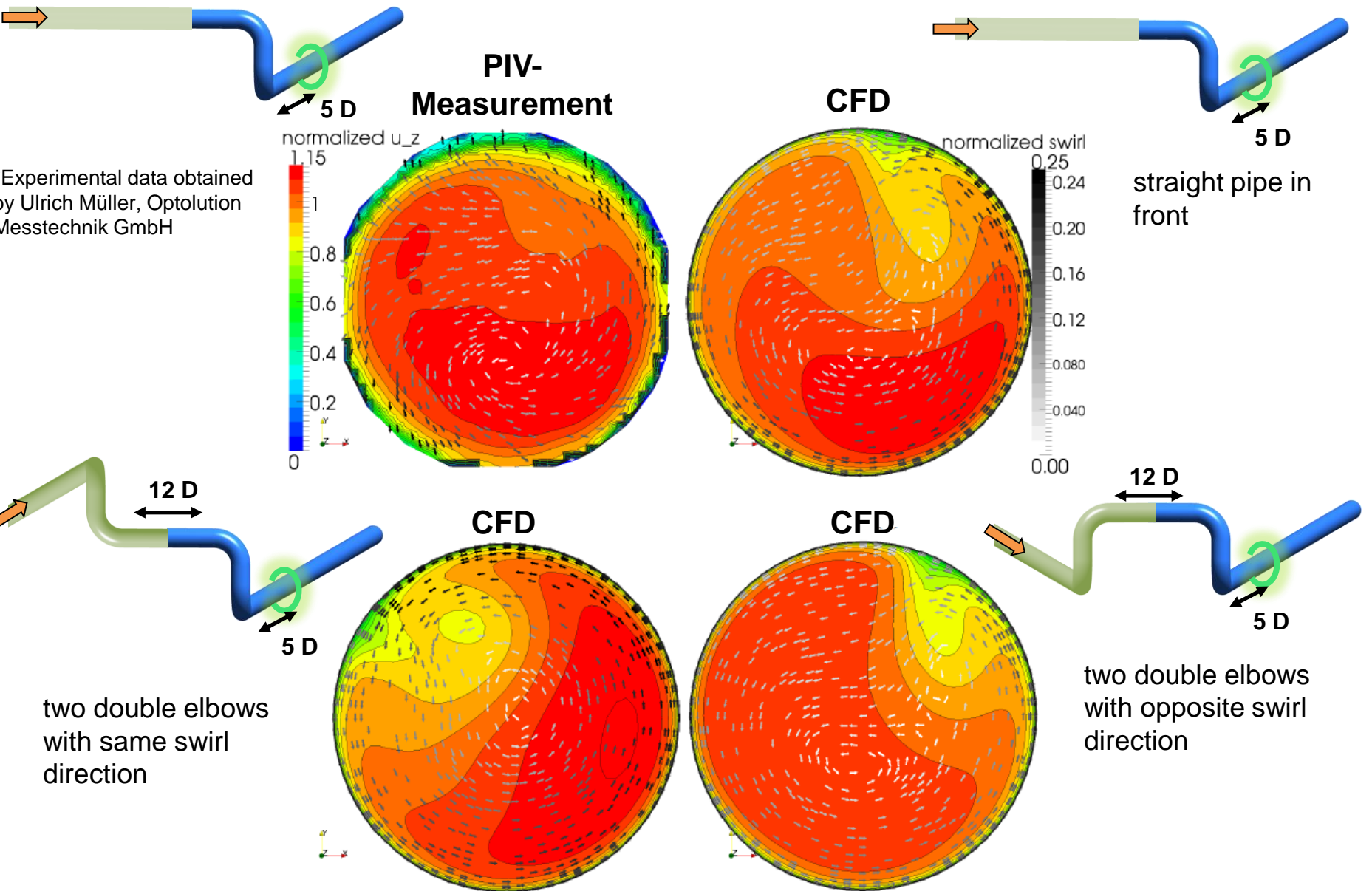
- pipe diameter 53.6 mm
- Re number = 3×10^5
- solver: Ansys CFX
- turbulence model: k- ω (wilcox 1986)

Mesh:

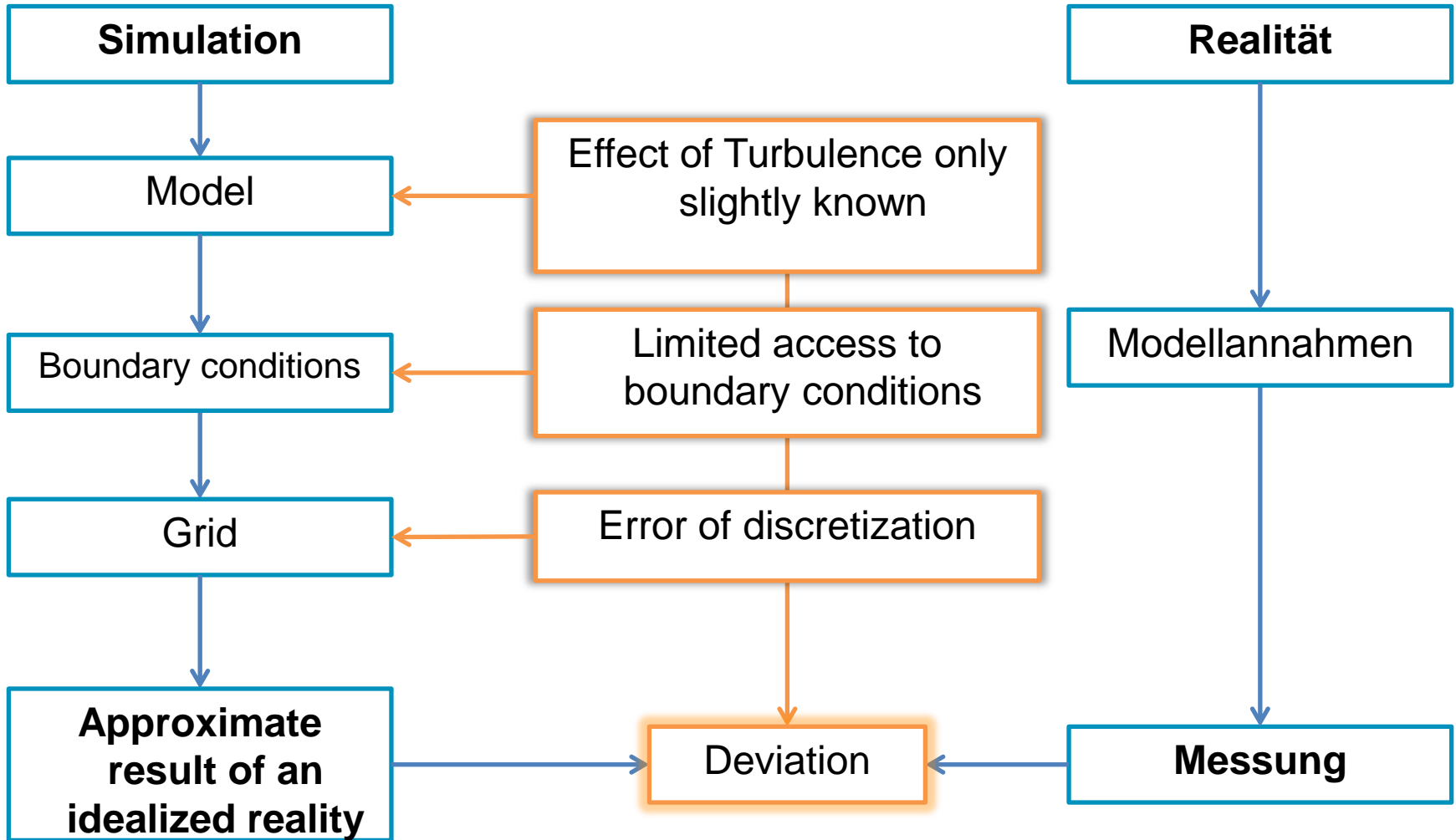
- structured hexahedral O-grid 3.2 mil. elements
- wall distance $y^+ = 1$

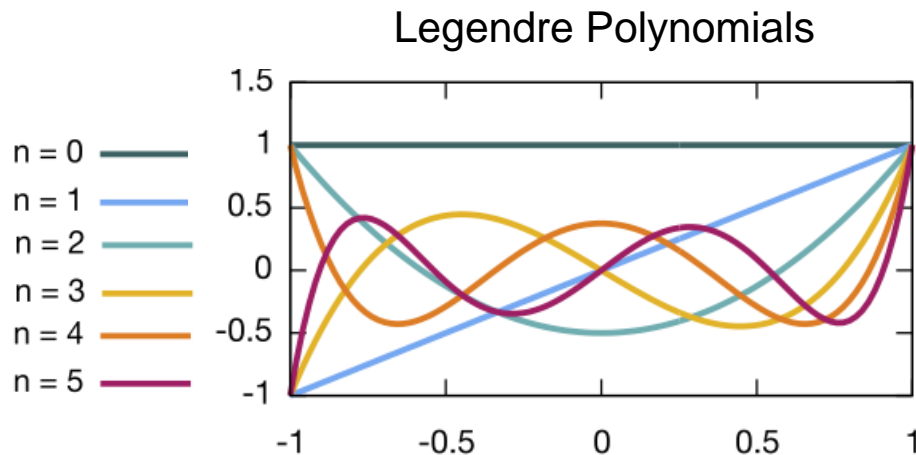
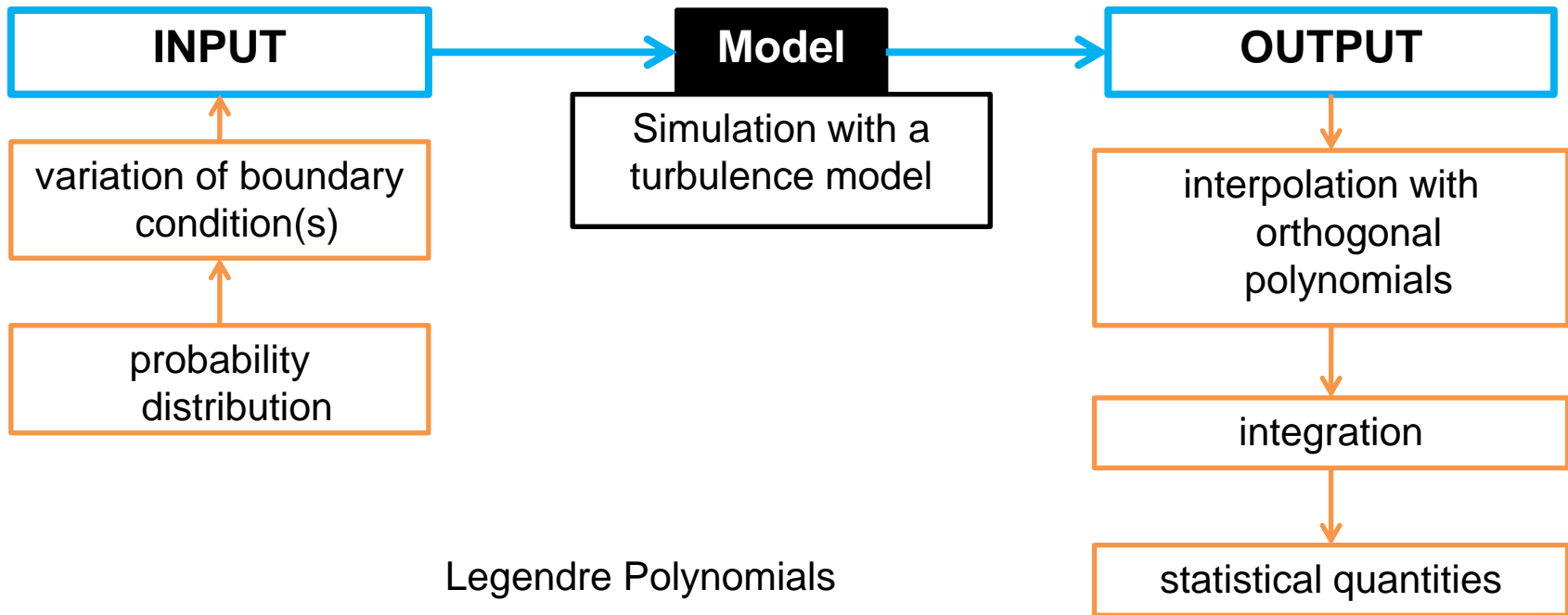


Sensitivity of a double elbow out-of-plane



Vergleichbarkeit von Messung und Simulation



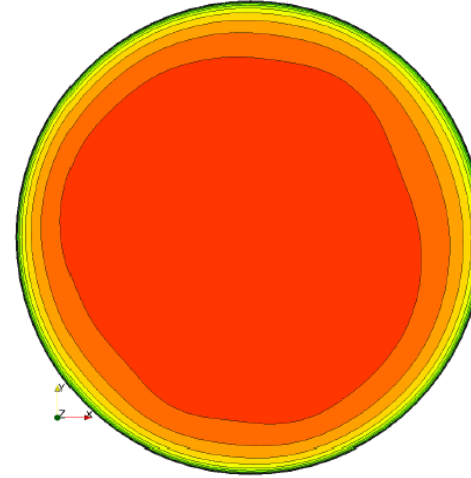
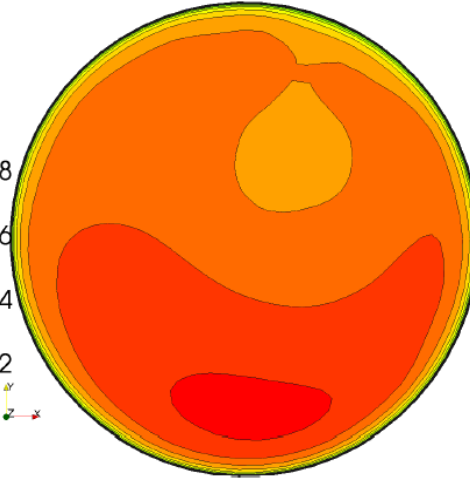
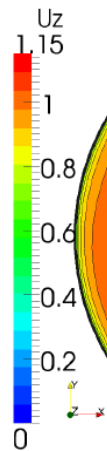


**Faster convergence
then Monte Carlo
methods!**

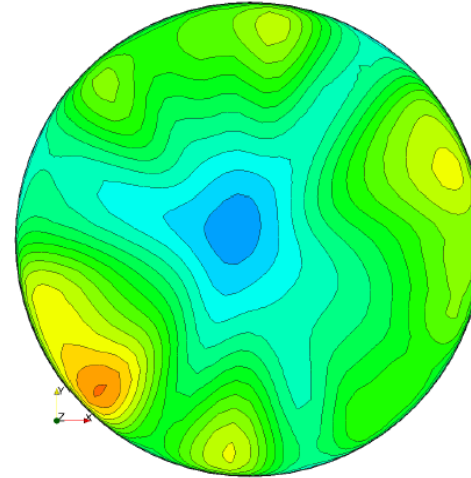
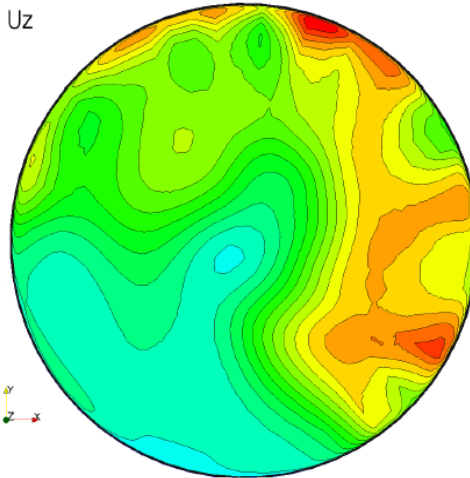
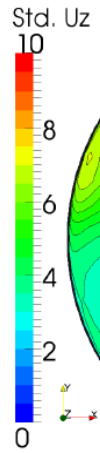
5 D distance

17 D distance

Mean
(Expectation)
Value



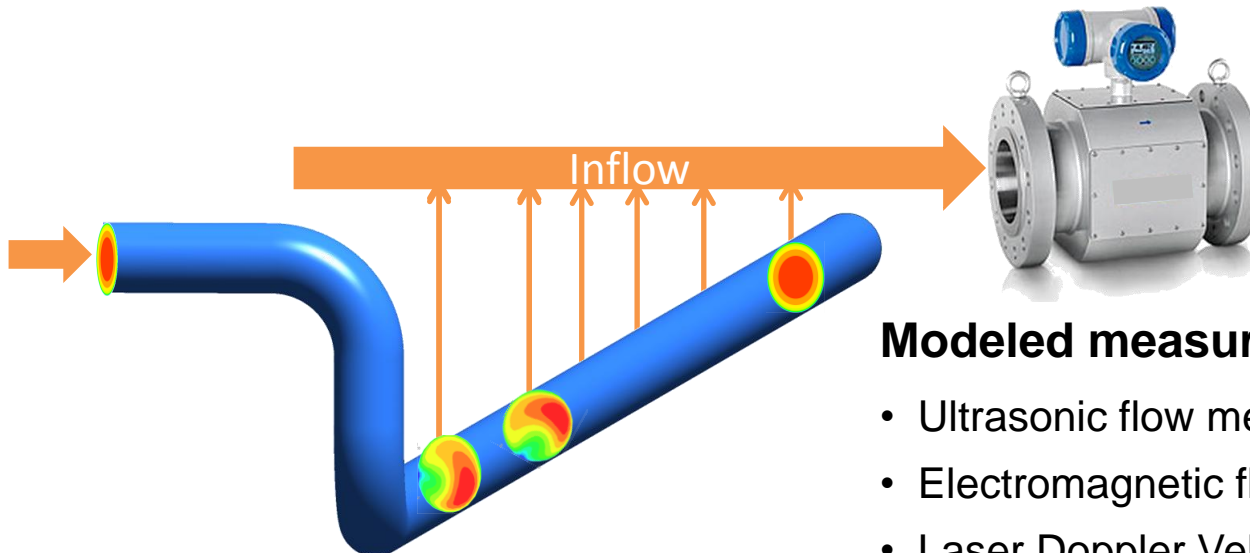
Standard
deviation



- CFD can capture the main qualitative effects seen in the experiment
- Profiles are sensitive to the inflow conditions
- The azimuthally position of the asymmetry is varying

Next step:

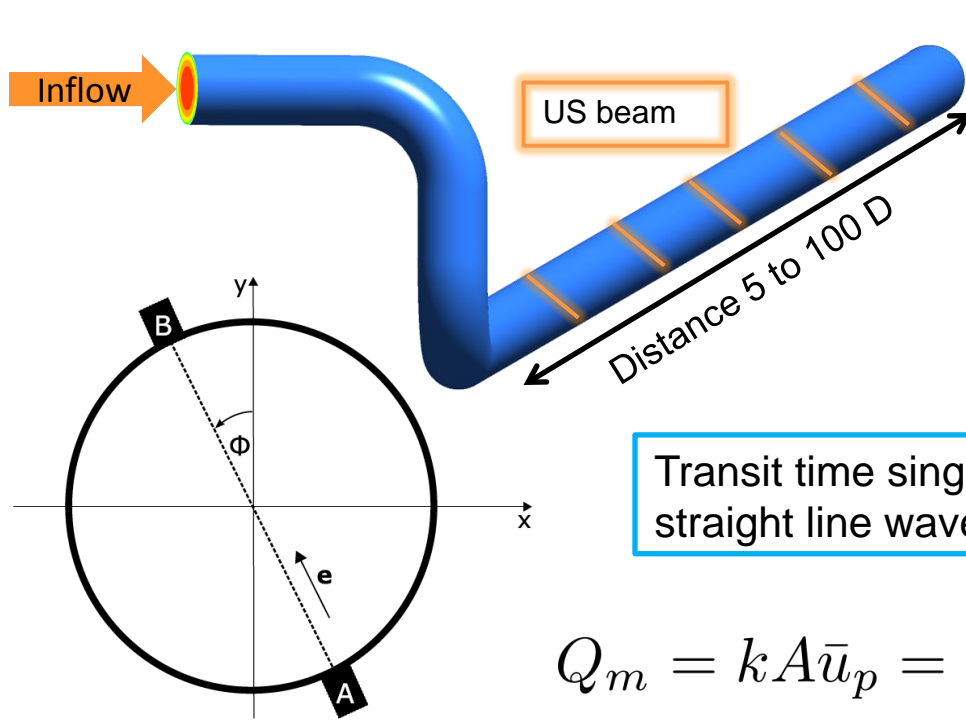
- Modeling the measurement principle of a flow meter
- Define the angular position of the flow meter as random
- Quantify uncertainties of the Flow meter with Polynomial Chaos



Modeled measurement principles:

- Ultrasonic flow meter
- Electromagnetic flow meter
- Laser Doppler Velocimeter

Sensitivity of an ultrasonic flow meter



Random angular position ϕ

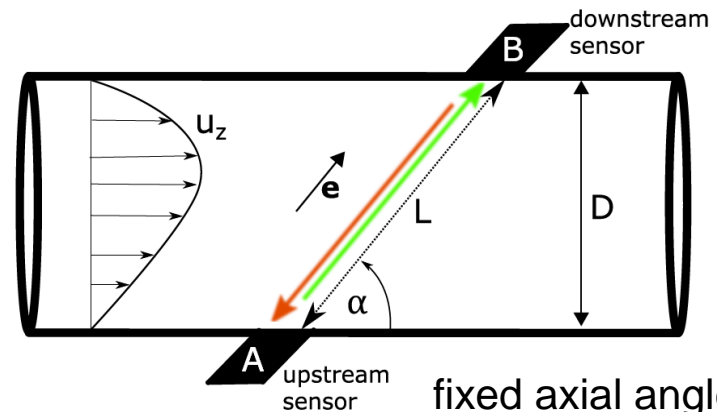
Transit time single beam with straight line wave propagation

$$Q_m = kA\bar{u}_p = \frac{kA}{Le_z} \int_0^L u(l) e dl$$

$$u = (u_r, u_\phi, u_z)$$

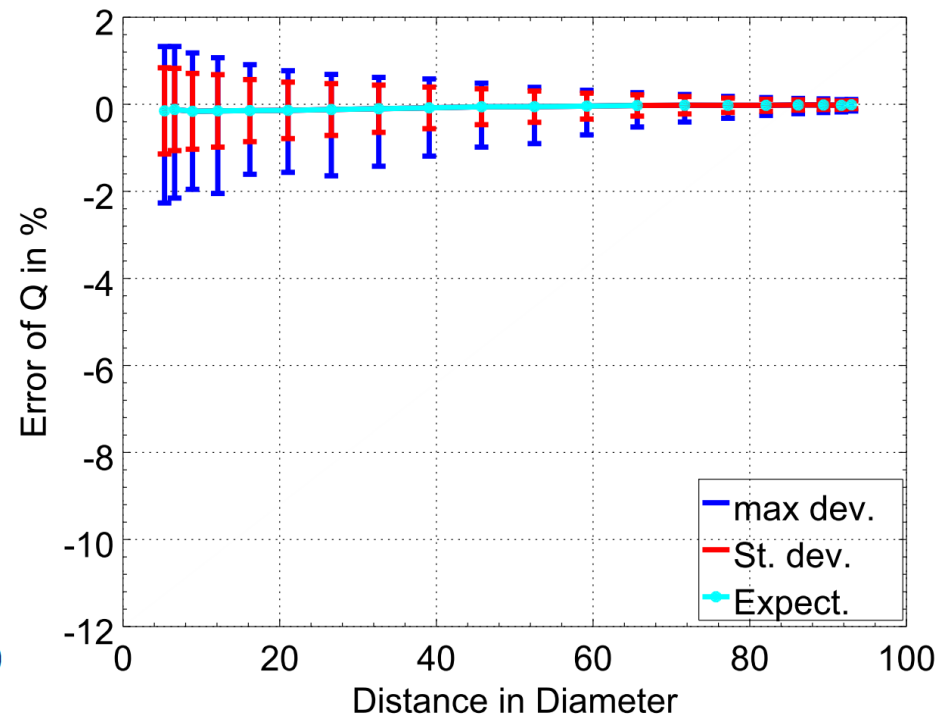
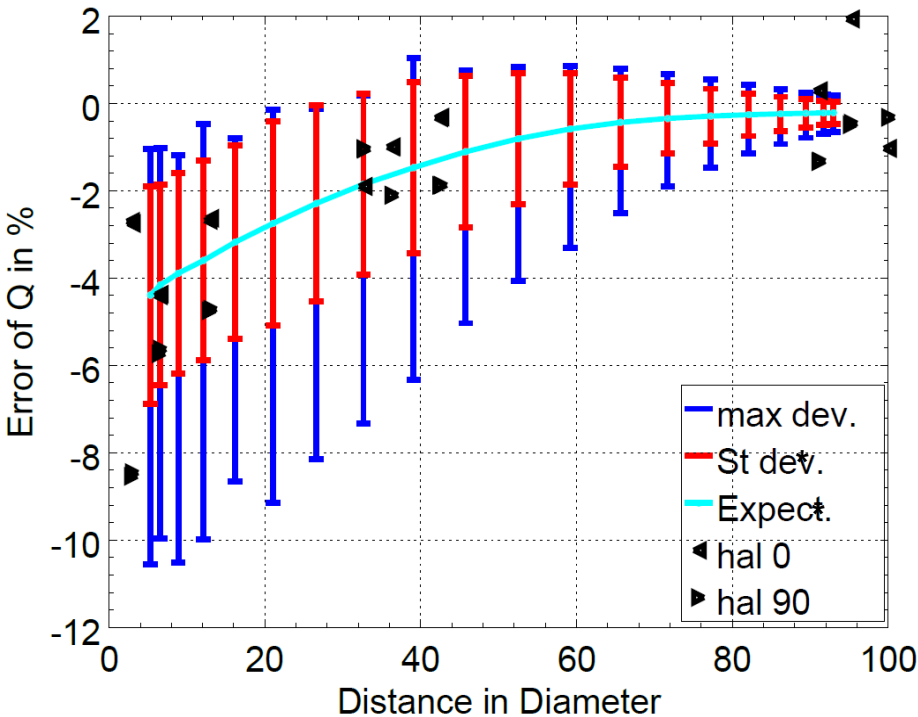
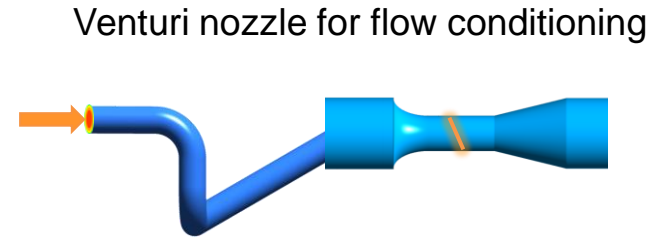
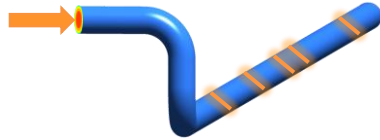
$$e = (\sin(\alpha), 0, \cos(\alpha))^T$$

$$\text{Error in } \% = \varepsilon = \frac{100}{Q_{real}} (Q_m - Q_{real})$$



fixed axial angle $\alpha = 45^\circ$

Sensitivity of an ultrasonic flow meter



* Halttunen, J., 1990. Installation effects on ultrasonic and electromagnetic flowmeters: a model-based approach. Flow Measurement and Instrumentation 1, 287-292

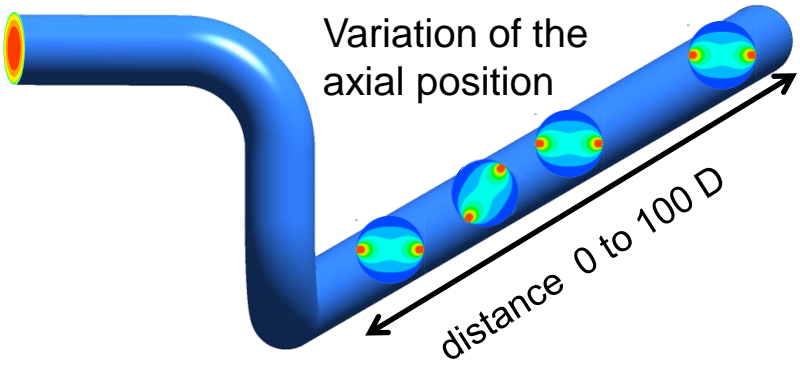
* Mattingly, G. E., Yeh, T. T., 4-7 June 1990. Secondary flow effects due to several elbow configurations. In: ASME Fluid Measurement and instrumentation Forum 1990, Toronto, Ontario, Canada

Sensitivity of an electromagnetic flow meter

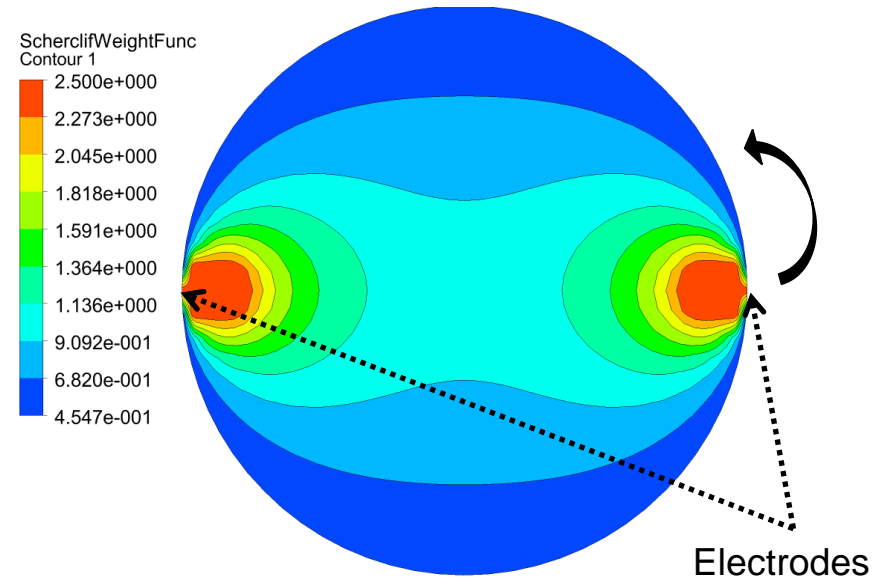
Weight function (Shercliff)

$$Q(z) = k_m \int_z^{z+l} \iint_A W(x, y) u_z(x, y, z) dA$$

$$W(x, y) = \frac{R^4 + R^2(x^2 - y^2)}{R^4 + 2R^2(x^2 - y^2) + (x^2 + y^2)^2}$$

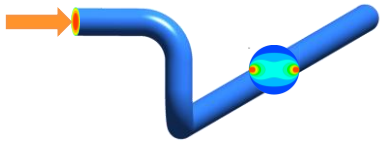


Variation of the angular position of the electrodes 0° to 360°

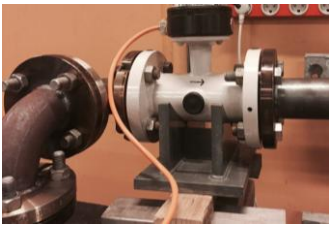
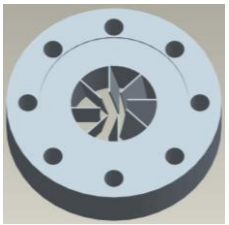
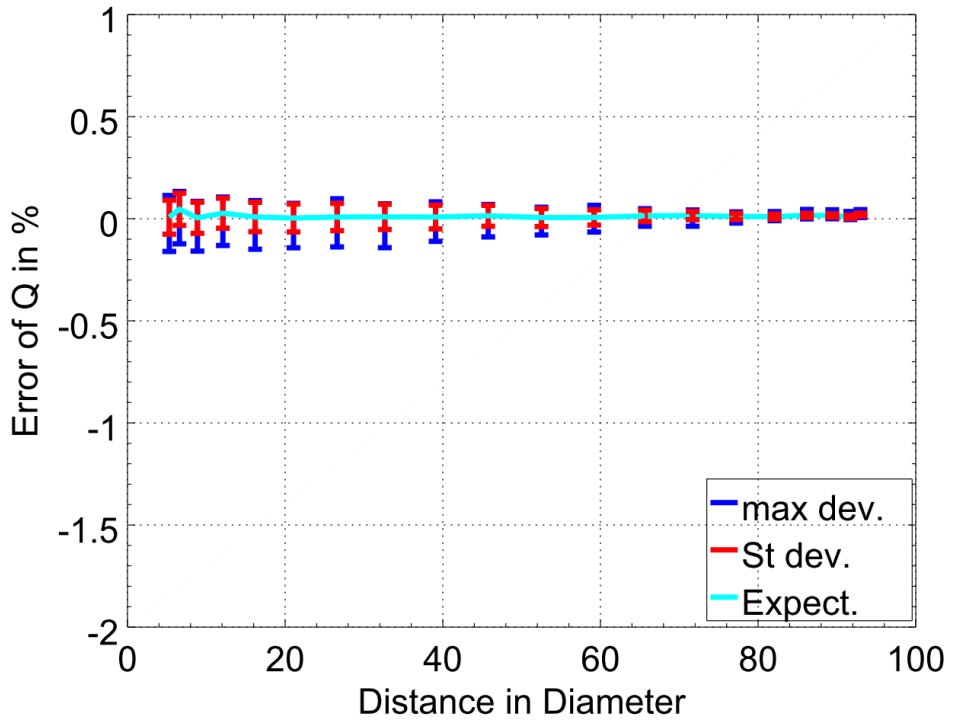
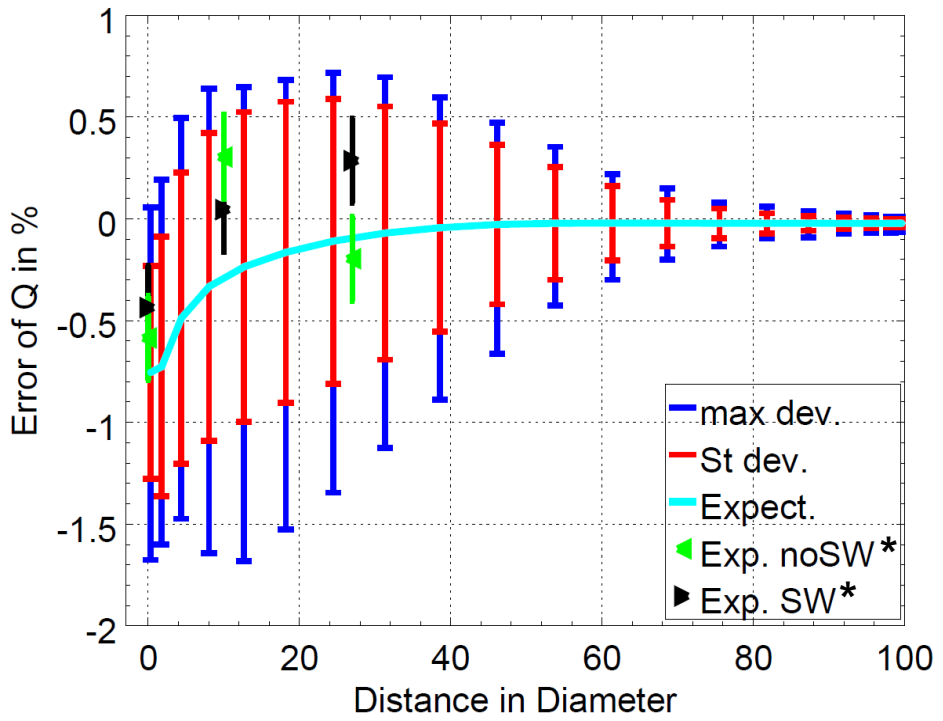
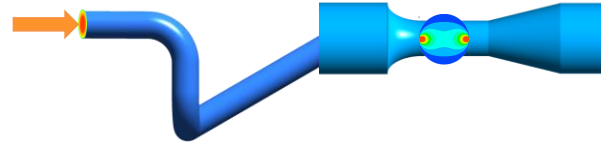


$$\text{Error in \%} = \varepsilon = \frac{100}{Q_{real}} (Q_m - Q_{real})$$

Sensitivity of an electromagnetic flow meter



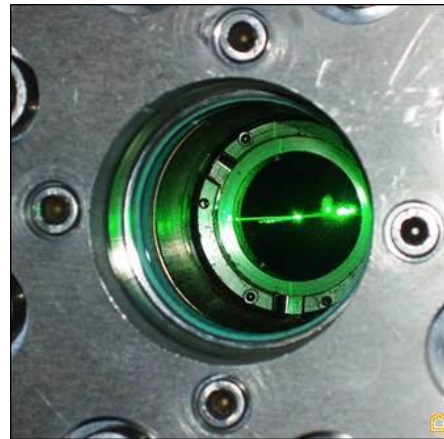
Venturi nozzle for flow conditioning



*Experimental data obtained by J. B. Kondrup, FORCE Technology, Denmark



drilling procedure certified for district heating applications (“hot tapping”)



contour-fitting window on the interior surface of the pipe



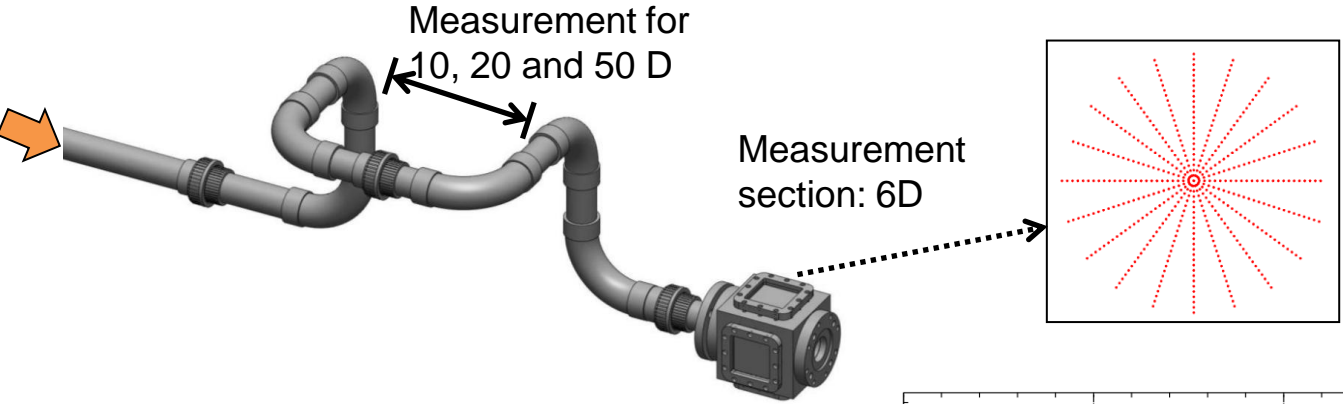
mobile Laser Doppler velocimeter

The flow rate is calculated by the integral of the axial velocity along a single path

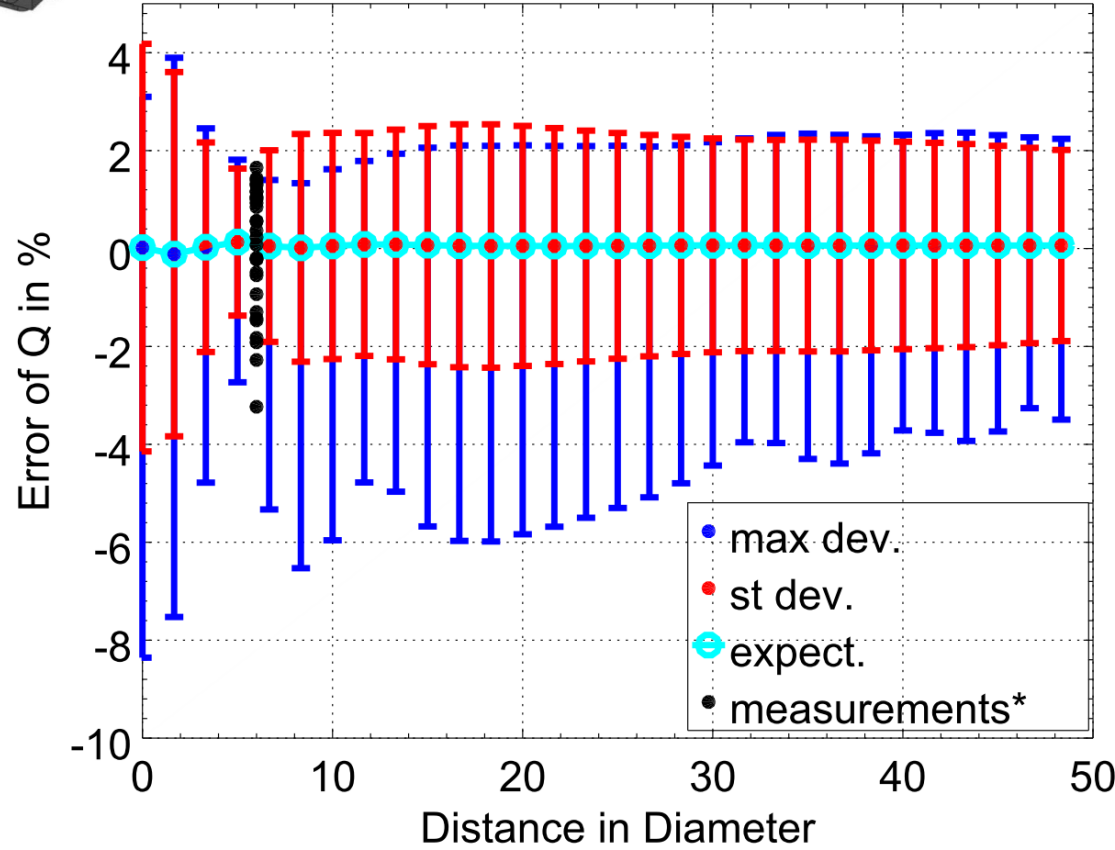
$$Q_m = \pi \int_{-R}^R u(r) |r| dr$$

$$\text{Error in } \% = \varepsilon = \frac{100}{Q_{real}} (Q_m - Q_{real})$$

Uncertainty of a laser Doppler velocimeter



Three measurements with each 10 path for each path the flow rate is calculated



*Experimental data obtained by A. Swienty and Phillip Kretschmer, TU-Berlin, Department of Fluid System Dynamics

- Sensitivity of flow profiles behind double elbows out-of-plane was demonstrated
- Uncertainty of electromagnetic and ultrasonic flow meters can be quantified with simple RANS models
- A Venturi nozzle bring huge improvement for the measurement accuracy
- Uncertainty for single path laser Doppler measurements can be quantified

Publications:

- A. Weissenbrunner, A. Fiebach et. al, 2016, Simulation-based determination of systematic errors of flow meters due to uncertain inflow conditions, Flow Measurement and Instrumentation, <http://dx.doi.org/10.1016/j.flowmeasinst.2016.07.011>
- S. Schmelter, A. Fiebach, A. Weissenbrunner, 2016, Polynomchaos zur Unsicherheitsquantifizierung in Strömungssimulationen für metrologische Anwendungen, Technisches Messen 2016; 83(2): 71–76
- A. Weissenbrunner et. al, 2016, A coupled numerical and laser optical method for on-site calibration of flow meters in district heating, in preparation



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